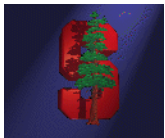

AA 284a
Advanced Rocket Propulsion

Lecture 16
Rocket Testing

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Stanford University

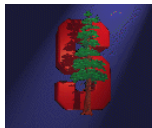


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Rocket Testing

- The physical and chemical phenomena that take place in a rocket system is very complex and comprehensive models to reliably design a new system or predict the performance of a new design do NOT exist.
- This requires an extensive testing effort in the development process
- Testing should be conducted in conjunction with a comprehensive modeling/simulation activity.
- The performance parameters that are of interest for a rocket system are
 - c^* and I_{sp} efficiencies
 - Regression rates for solid and hybrid rockets
 - Stability character (See Lecture 14)
 - Injector performance (See Lecture 12)
 - Nozzle erosion rates (for ablative nozzles)
 - Nozzle cooling system performance (for cooled nozzles)



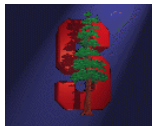
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Rocket Testing – Efficiency Estimation

- Determination of the efficiencies from motor/engine test data
- c^* efficiency can be calculated using the following set of equations (chamber pressure integral method) – derived from c^* equation

$$c_{act}^* = \frac{C_d \bar{A}_n \int_0^{t_b} P_c dt}{(\Delta M_{ox} + \Delta M_f + \Delta M_{in})} \quad \eta_c = \frac{c_{act}^*}{c_{theo}^*} \quad O/F = \Delta M_{ox} / \Delta M_f$$

- Note that the theoretical c^* can be calculated using the average chamber pressure, and average oxidizer to fuel ratio
 - One must assume frozen or shifting equilibrium in this calculation
 - This assumption would change the numerical value of the efficiency
 - Frozen equilibrium assumption results in higher than actual efficiencies
 - Shifting equilibrium assumption results in lower than actual efficiencies
- Discharge coefficient of the nozzle can be obtained from cold gas flow test
- Nozzle area is the average value for the test



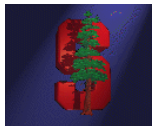
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Rocket Testing - Efficiency Estimation

- Isp efficiency can be calculated using the following set of equations (thrust integral method)

$$(I_{sp})_{act} = \frac{\int_0^{t_b} T dt}{g_o (\Delta M_{ox} + \Delta M_f + \Delta M_{in})} \quad \eta_{Isp} = \frac{(I_{sp})_{act}}{(I_{sp})_{theo}}$$

- Note that the theoretical Isp can be calculated using the average chamber pressure, average oxidizer to fuel ratio and the nozzle area ratio
 - One must assume frozen or shifting equilibrium in this calculation
 - This assumption would change the numerical value of the efficiency
 - Frozen equilibrium assumption results in higher than actual efficiencies
 - Shifting equilibrium assumption results in lower than actual efficiencies



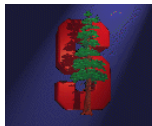
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Rocket Testing – Regression Rate Estimation

- For hybrid or solid rockets with circular ports
- Space time averaged regression rate can be estimated using the following equations

$$\bar{r} = \frac{d_f - d_i}{2 t_b} \quad d_f = \left[d_i^2 + \frac{4\Delta M_f}{\pi\rho_f L_g} \right]^{1/2}$$

- Estimating the final diameter from the fuel mass loss results in final diameters that are more accurate than the directly measured values.
- Burn time can be defined as the action time
 - From the moment that 50% of the full pressure is achieved
 - To the moment that 50% of the full pressure is lost
- Selection of burn time is critical for accurate measurement
 - For short tests the transients dominate
 - For long tests the flux variation is too large (for hybrids)



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Rocket Testing – Oxidizer Mass Flux

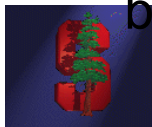
- In a hybrid rocket oxidizer mass flux has to be estimated
- First a flow rate measurement required
 - Average from a direct measurement of the flow rate (i.e. turbine flow meter)
 - Or from oxidizer tank weight measurement

$$\bar{\dot{m}}_{ox} = \frac{\Delta M_{ox}}{t_b}$$

- Three methods of defining average flux is possible (always specify the method used in the calculation)
- The most accurate one is based on average diameter

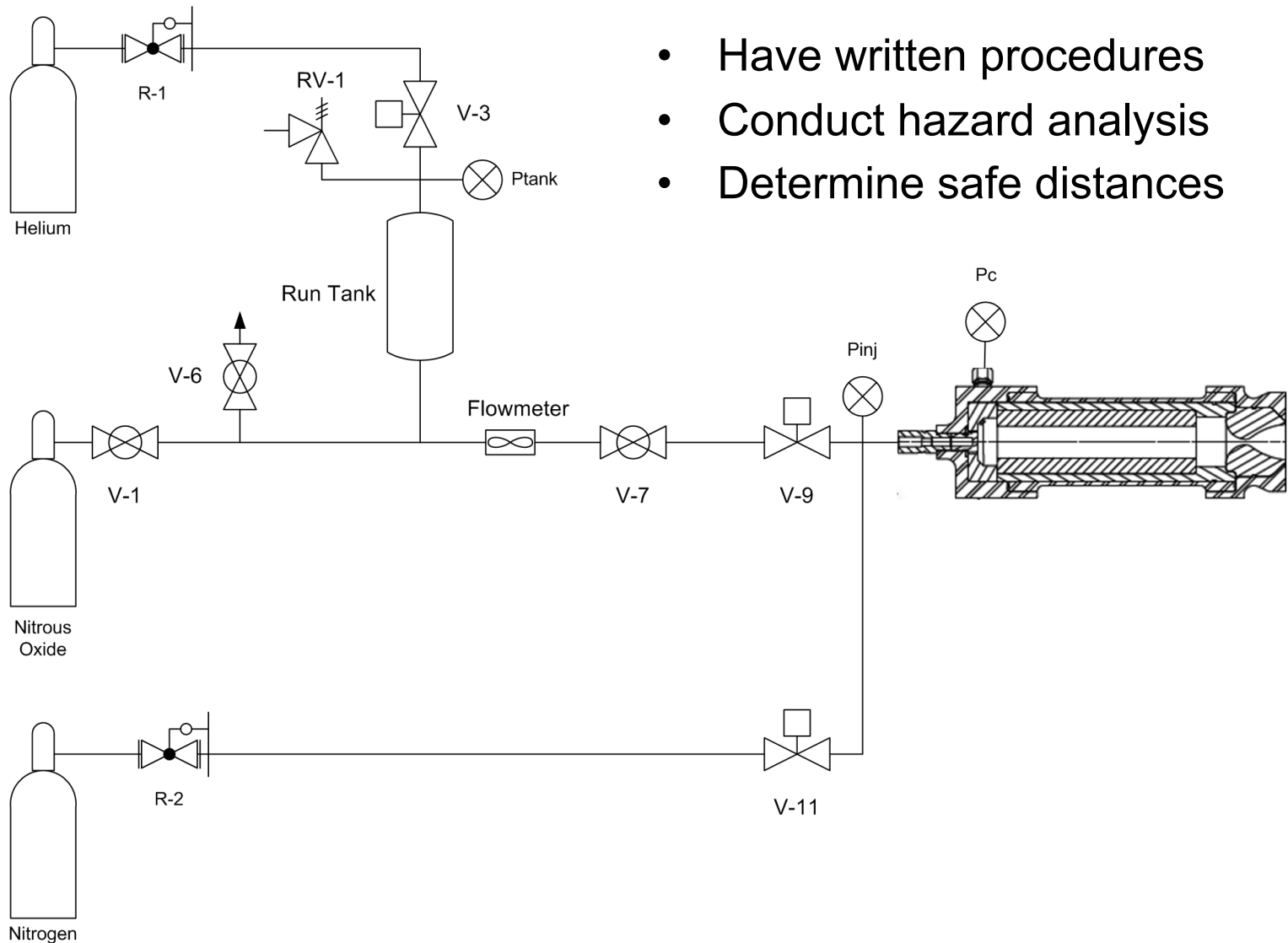
$$\bar{G}_{ox} = \frac{16 \bar{\dot{m}}_{ox}}{\pi(d_i + df)^2}$$

- Each motor test generates a regression rate oxidizer mass flux pair. At least 10-15 tests should be used to establish the regression rate law for a propellant combination. Length and pressure effects should also be evaluated by additional testing.

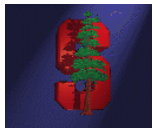


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Rocket Testing – P&ID Diagram for a Hybrid Rocket



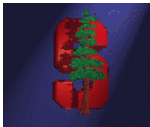
- Have written procedures
- Conduct hazard analysis
- Determine safe distances



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Rocket Testing – Measured Quantities

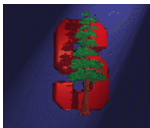
- Thrust Force:
 - Use a set of load cells to measure forces in the axial and lateral directions
 - Always conduct an *in situ* calibration by applying a known force to the fully assembled configuration and measuring the voltage output.
 - Note that the effect of oxidizer flow into the motor on the thrust measurement accuracy in a gaseous system is significant
 - For most liquid oxidizer systems 1-2% accuracy is achievable
- Pressures:
 - Combustion chamber (multiple locations, pre and post combustion chambers)
 - Injector upstream
 - Oxidizer tank
 - Use two kinds of transducers simultaneously
 - Fast responding for dynamic measurements (i.e. Kistler). Major DC shift
 - Slow responding with high DC accuracy (i.e. GEM). Poor dynamic response
 - Better than 1% accuracy is easily achievable



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Rocket Testing – Measured Quantities

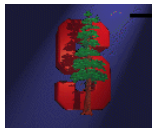
- Oxidizer (and liquid fuel) Flow Rate:
 - This is one of the most difficult measurements (>5% accuracy is common)
 - The following techniques can be used for this purpose
 - Tank weight (gas or liquid) Change in the tank weight
 - Easiest method to directly measure mass flow rate
 - Generally not very accurate or reliable due to zero shift during testing.
 - No transient measurements
 - Turbine flow meter. (gas or liquid) Turbine spinning in a pipe
 - This is a volumetric flow measurement.
 - Inaccuracies due to the estimation of the density
 - Can not be used in a two phase flow situation
 - Fast response
 - Venturi flow meter (gas or liquid); Pressure change in a venturi
 - Small range of flow rates
 - Inaccuracies due to the estimation of the density
 - Can not be used in a two phase flow situation
 - Coriolis Flow meter (gas or liquid) Coriolis force acting on a looping pipe
 - Very accurate. Direct mass flow rate measurement
 - Quite expensive
 - Generally slow response



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Rocket Testing – Measured Quantities

- Temperatures:
 - Measure temperatures in
 - Feed lines
 - Injector upstream
 - Inside the combustion chamber (very difficult)
 - Outside wall of the chamber or nozzle
 - Use thermocouples (2-3 C accuracy). Make sure to use the TC types with the correct temperature range
 - LOX lines (90-120 K)
 - Chamber: (2000-3000 K)
 - Most TC's are very slow in responding to changes in temperature
- Port Diameter:
 - Inside micrometers, T-scopes (accurate to 0.002"-0.005")
 - Laser systems
- Fuel Mass
 - Scales (before and after test)
 - This could be a highly accurate measurement



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Rocket Testing – Measured Quantities

- High Speed Video of the plume and motor/engine:
 - Video recording at speeds of 1000 frames per second is very useful
 - Plume events can be used to construct the failures or anomalous behavior.
- Filtering:
 - Use analog filters for anti-aliasing purposes
 - Cut off frequency selected to resolve up to the 3rd – 4th longitudinal mode for a hybrid. For liquids sampling rate should be much faster (radial and tangential modes)
- Data Acquisition:
 - Sampling rate should be selected at least 4 times the maximum frequency of interest
 - A 16 bit DAQ board have reasonable resolution for most systems.

