

6.4 Radiation beam targeting a cancer cell (two-axis machine).

The following shows a radiation machine consisting of a rigid emitter B and a circular gimbal A . Emitter B is connected by a small one-axis revolute “targeting” motor to gimbal A at point B_o . Gimbal A rotates relative to the treatment room N because of a **constant-speed** revolute motor that connects A to N at point N_o and causes B_o to move with **constant-speed** in a circle centered at point N_o of N . Note: Both revolute motor axes are perpendicular to the circle traced out by B_o .

A thin radiation ray is emitted from B_o to target a cancer cell Q that moves (e.g., because of respiration and circulation) along a line that passes through points Q_i and Q_f of a patient who is otherwise motionless in a treatment room N . Note: Line segment $\overline{Q_i Q_f}$ is perpendicular to the revolute motors’ axes.

Description	Symbol	Type	Value
Horizontally-right measure of Q_i 's position vector from N_o	x_i	Constant	10 cm
Vertically-upward measure of Q_i 's position vector from N_o	y_i	Constant	1 cm
Horizontally-right measure of Q_f 's position vector from N_o	x_f	Constant	20 cm
Vertically-upward measure of Q_f 's position vector from N_o	y_f	Constant	2 cm
Patient respiration rate (15 breaths/minute)	ω_r	Constant	$\frac{2\pi}{4} \frac{\text{rad}}{\text{sec}}$
Radius of circular gimbal A	R	Constant	40 cm
Angle between downward vertical and B_o 's position vector from N_o	θ_A	Specified	$\frac{2\pi}{360} t \frac{\text{rad}}{\text{sec}}$
Angle between upward vertical and Q 's position vector from B_o	θ_B	Variable	

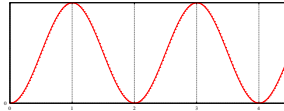
Horizontally-right is generally directed from the patient's left to right shoulder.

Vertically-upward is generally directed from the patient's posterior to anterior.

θ_A is **counter-clockwise positive** whereas θ_B is **clockwise positive**.

The cancer cell moves from Q_i to Q_f with displacement

$$s = \frac{A}{2} [1 - \cos(\omega_r t)]$$



where A , the distance between Q_i and Q_f , is

$$A = \sqrt{(x_f - x_i)^2 + (y_f - y_i)^2}$$

Determine θ_B at $t = 0$ and $t = 60$ sec (3 significant digits).

Plot θ_B° for $0 \leq t \leq 360$ sec with data every 0.25 sec.

See Section 2.5.5 and ensure θ_B is continuous to reflect a real motor.

Result:

$$\theta_B|_{t=0} = 13.7^\circ \quad \theta_B|_{t=60} = -49.6^\circ$$

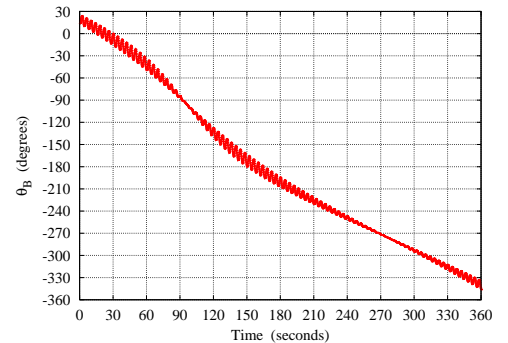
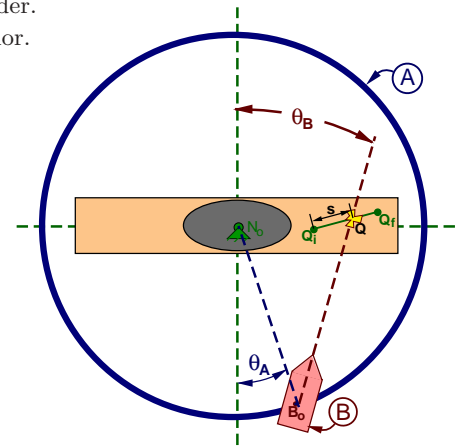
Maximum torque specification helps properly size a motor.

Knowing the targeting motor's torque is $I \ddot{\theta}_B$ ($I = 2 \text{ g m}^2$)

determine its maximum absolute value (1^+ significant digit).

Result:

$$|\mathbf{T}_{\max}| = 0.83 \text{ milliNewton m}$$



An alternate treatment strategy is to lock θ_A and θ_B so radiation targets Q at the midpoint of line segment $\overline{Q_i Q_f}$. The sensitivity and ease of targeting depends on the angle between the radiation and $\overline{Q_i Q_f}$. Determine sets of values for θ_A and θ_B to deliver radiation perpendicular or parallel to $\overline{Q_i Q_f}$ (3^+ significant digits). Complete the table with $0^\circ \leq \theta_A \leq 360^\circ$ and $-360^\circ \leq \theta_B \leq 0^\circ$.

Result:

Solution #	Perpendicular to $\overline{Q_i Q_f}$		Parallel to $\overline{Q_i Q_f}$	
1	$\theta_A = 27.9^\circ$	$\theta_B = -5.71^\circ$	$\theta_A = 95.7^\circ$	$\theta_B = -95.7^\circ$
2	$\theta_A = 163.6^\circ$	$\theta_B = -185.7^\circ$	$\theta_A = 275.7^\circ$	$\theta_B = -275.7^\circ$