

Dipole Antennas

EE252

$$\bar{A} = \frac{\mu}{4\pi} \int_{\text{vol}} \bar{J}(\vec{r}') \frac{e^{-jkR}}{R} d\tau' \xrightarrow{\sim} \underbrace{\frac{\mu}{4\pi} \int_{z=-l/2}^{z=l/2} I(z') \frac{e^{-jkR}}{R} dz'}_{\text{for a fine wire element}}$$

for a fine wire element

$$\bar{E} = -j\omega \bar{A} + \frac{\nabla(\nabla \cdot \bar{A})}{j\omega \mu_0 \epsilon_0} \rightarrow \underbrace{-j\omega \bar{A}_T}_{\text{far-field}}$$

far-field

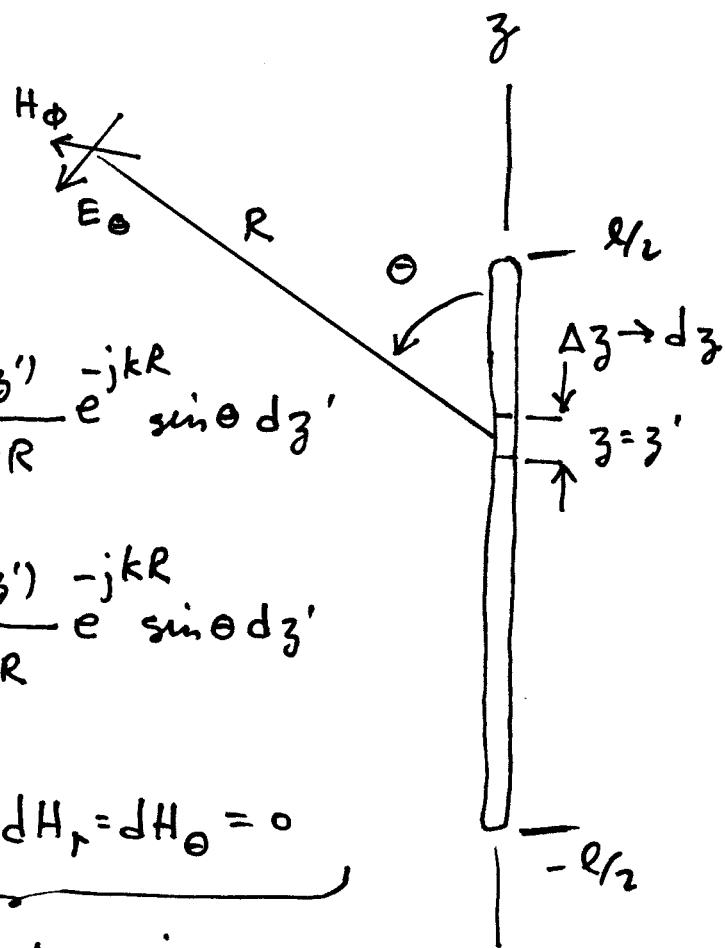
...

$$dE_\theta = j\eta k \frac{I(z')}{4\pi R} e^{-jkR} \sin\theta dz'$$

$$dH_\phi = jk \frac{I(z')}{4\pi R} e^{-jkR} \sin\theta dz'$$

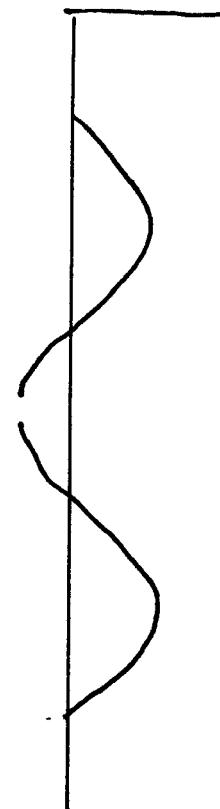
$$dE_r = dE_\phi = dH_r = dH_\theta = 0$$

all in the far-field



Example

$I(z)$



1...

Far-field Approximations

$$E_\theta = \int_{-l/2}^{l/2} dE_\theta = j \frac{\gamma k e^{-jkr}}{4\pi r} \int_{-l/2}^{l/2} I(z') e^{+jkz' \cos \theta} dz'$$

$\underbrace{\phantom{\int_{-l/2}^{l/2} dE_\theta}}$ element factor $\underbrace{\phantom{e^{+jkz' \cos \theta}}}_{-l/2} \phantom{\int_{-l/2}^{l/2} dz'}$ space factor

$$I(z') = I_0 \sin[k(l/2 - z')] \quad 0 \leq z' \leq l/2$$

$$I_0 \sin[k(l/2 + z')] \quad -l/2 \leq z' < 0$$

1. . .

$$\int I(z') e^{jk \cos \theta z'} dz' = ?$$

form is $\int e^{\alpha z} \sin(\beta z + \gamma) dz$ with

$$\alpha = j k \cos \theta, \quad \beta = \pm k, \quad \gamma = \frac{k\ell}{2} = \frac{\pi\ell}{J}$$

use two step integration by parts ($u dv = uv - v du$)

begin with ... $u = \sin(\beta z + \gamma) \quad du = \beta \cos(\beta z + \gamma)$

$$dv = e^{\alpha z} dz \quad v = \frac{1}{\alpha} e^{\alpha z}$$

/ ... A short while later ...

$$E_\theta = j \eta \frac{I_0 e^{-jkr}}{2\pi r} \left[\frac{\cos\left(\frac{k}{2}l \cos\theta\right) - \cos\left(\frac{k}{2}l\right)}{\sin\theta} \right]$$

$$E_\phi = j \eta \frac{I_0 e^{-jkr}}{2\pi r} F(\theta)$$

$$H_\phi = \frac{E_\theta}{\eta} = j \frac{I_0 e^{-jkr}}{2\pi r} F(\theta)$$

$\left. \begin{array}{l} \text{all valid} \\ \text{in far-} \\ \text{field with} \\ \text{Dipole length} \\ "l" \end{array} \right\}$

what about power radiated from dipole

$$\bar{W}_{\text{Ave}} = \frac{1}{2\eta} |E_\theta|^2 \hat{a}_r = \gamma \frac{|I_0|^2}{8\pi^2 r^2} \cdot |F(\theta)|^2$$

$$\bar{U} = r^2 \bar{W}_{\text{Ave}} = \gamma \frac{|I_0|^2}{8\pi^2} |F(\theta)|^2$$

$$F(\theta) \Big|_{\theta=0} = ? \quad (\text{L'Hopital's Rule}) = 0$$

Never any radiation off
the end !!
/...

How about broadside to the dipole?

$$\frac{d}{d\theta} \left[|F(\theta)|^2 \right] = 0 \quad \text{if } k \ll 1,$$

$\theta = \{$

So broadside $|F(\theta)|^2$ is either a
maximum $\underline{\text{or}}$ a minimum

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Short Dipole

$$\bar{W}_{\text{Ave}} \rightarrow \frac{\gamma |I_0|^2}{8\pi^2 r^2} \left[\frac{\cos\left[\frac{kl}{2} \cdot \cos\theta\right] - \cos\left[\frac{kl}{2}\right]}{\sin\theta} \right]^2$$

$$\frac{kl}{2} \rightarrow r \ll 1$$

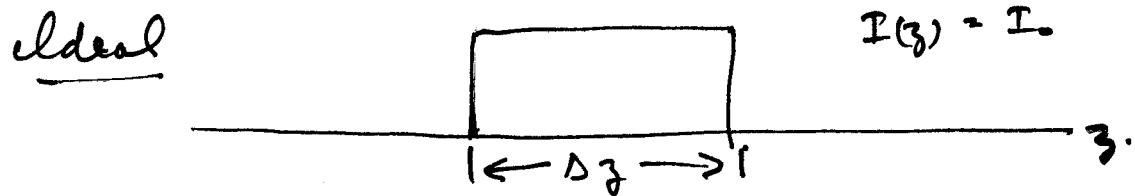
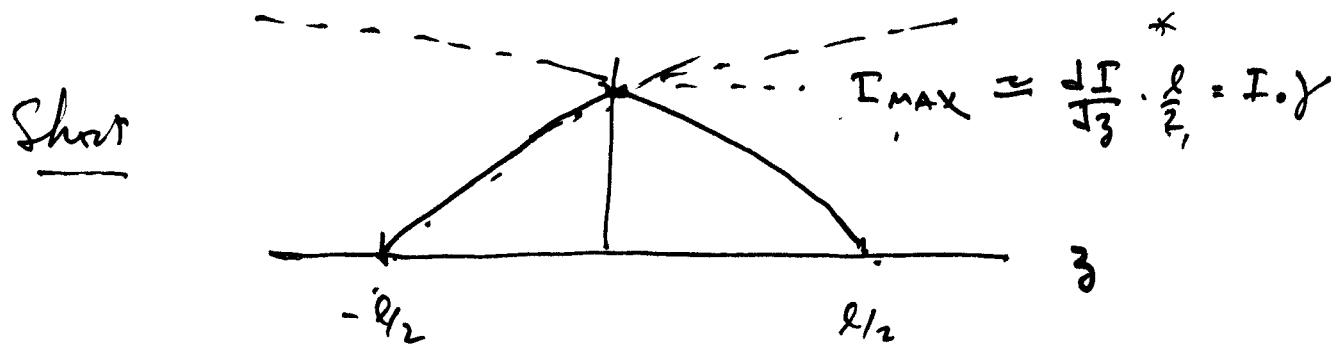
$$\bar{W}_{\text{Ave}} \approx \gamma \frac{|I_0|^2}{8\pi^2 r^2} \cdot \frac{\lambda^4}{4} \cdot \frac{(1 - \cos^2\theta)^2}{\sin^2\theta} = \gamma \frac{|I_0|^2}{8\pi^2 r^2} \frac{\lambda^4}{4} \sin^2\theta$$

$$\frac{kl}{2} \ll 1$$

$$= \frac{\gamma}{8} \left| \frac{I_0 \lambda}{\lambda} \right|^2 \left(\frac{2\pi l}{\lambda} \right)^2 \frac{\sin^2\theta}{r^2}$$

What is the difference between the "Short Dipole" & "ideal Dipole"?

Ans: the current distribution



$$* I(z) = I_0 \sin \left[\frac{k l}{2} - k |z| \right]$$

$$|\bar{W}_{\text{AVE}}| = \frac{\gamma}{8\pi^2 r^2} \cdot \left(\frac{I_0 \gamma}{2}\right)^2 \gamma^2 \sin^2 \theta$$

$$= \frac{\gamma}{8} \left(\frac{I_{\text{AVE}} \ell}{\lambda} \right)^2 \frac{\sin^2 \theta}{r^2}; \quad I_{\text{AVE}} = \frac{I_0 \gamma}{2}$$

Short dipole is not sensitive to the form of the current distribution, only to

$$\int_{-\ell/2}^{\ell/2} I(z) dz, \quad \text{for } \underline{\frac{\ell}{2} \ll \lambda}$$

If $\left[\frac{I_{\text{AVE}} \ell}{\lambda}\right] = \left[\frac{I_0 \Delta z}{\lambda}\right]$, short dipole is equivalent to an ideal dipole.

Short Dipole : Radiation Resistance

$$W_{\text{AVE}} = \frac{1}{8} \frac{1}{r^2} \left| \frac{I_{\text{AVE}} l}{\lambda} \right|^2 \sin^2 \theta$$

$$= \frac{15 \pi}{r^2} \left| \frac{I_{\text{AVE}} l}{\lambda} \right|^2 \sin^2 \theta$$

$$P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi W_{\text{AVE}} r^2 \sin \theta d\theta d\phi = 30\pi^2 \left[\frac{I_{\text{AVE}} l}{\lambda} \right]^2 \cdot \frac{4}{3}$$

$$= 40\pi^2 \left| \frac{I_{\text{AVE}} l}{\lambda} \right|^2 = \frac{1}{2} R_{\text{eff}} |I_{\text{MAX}}|^2 = 2R_{\text{eff}} |I_{\text{AVE}}|^2$$

short dip. / ...

$$\underbrace{R_{\text{eff}}}_{\text{short dipole}} = 20 \pi^2 \left(\frac{l}{\lambda} \right)^2 = \frac{1}{4} \underbrace{R_{\text{eff}}}_{\text{I.D.}} \text{ for an ideal dipole.}$$

Current is not used as effectively in a short dipole as it is in an ideal dipole!

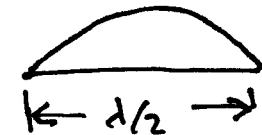
Aside: The 'trick' of 'top-loading' an antenna to increase the current on the radiating portion of the structure is based on the effect illustrated by the difference between the short and ideal dipoles. (135)
You can see this in practice at KNBR (near Foster City).

Half-wave Dipole ($l = \frac{\lambda}{2}$; $\frac{k_l}{2} = \frac{2\pi}{\lambda} \cdot \frac{l}{2} = \frac{\pi}{2}$)

$$E_\theta \approx j \eta \frac{I_0 e^{-jkr}}{2\pi r} \frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \quad I_0 = I_{\max},$$

for assumed
distribution

$$H_\phi \approx j \frac{I_0 e^{-jkr}}{2\pi r} \frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta}$$



$$W_{AVE} \approx \eta/2 \frac{|I_0|^2}{4\pi^2 r^2} \frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta}$$

1... $\lambda/2$ - Dipole

$$P_{\text{rad}} \approx \eta \left| \frac{I_0}{4\pi} \right|^2 \int_0^{\pi} \frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin \theta} d\theta = \eta \left| \frac{I_0}{4\pi} \right|^2 (1.219)$$

↑
numerically
determined factor

$$\approx \eta \left| \frac{I_0}{8\pi} \right|^2 \cdot (2.4)$$

$$\text{Directivity} = \frac{4\pi \frac{I_{\text{max}}}{P_{\text{rad}}}}{P_{\text{rad}}} = 4\pi \frac{\eta_0 \left| I_0 \right|^2 / 8\pi^2}{\eta_0 \left| \frac{I_0}{8\pi} \right|^2 \cdot (2.4)} = \frac{4}{2.4} = 1.64$$

which is only slightly greater ($9\frac{1}{3}\%$) than that
of an ideal dipole

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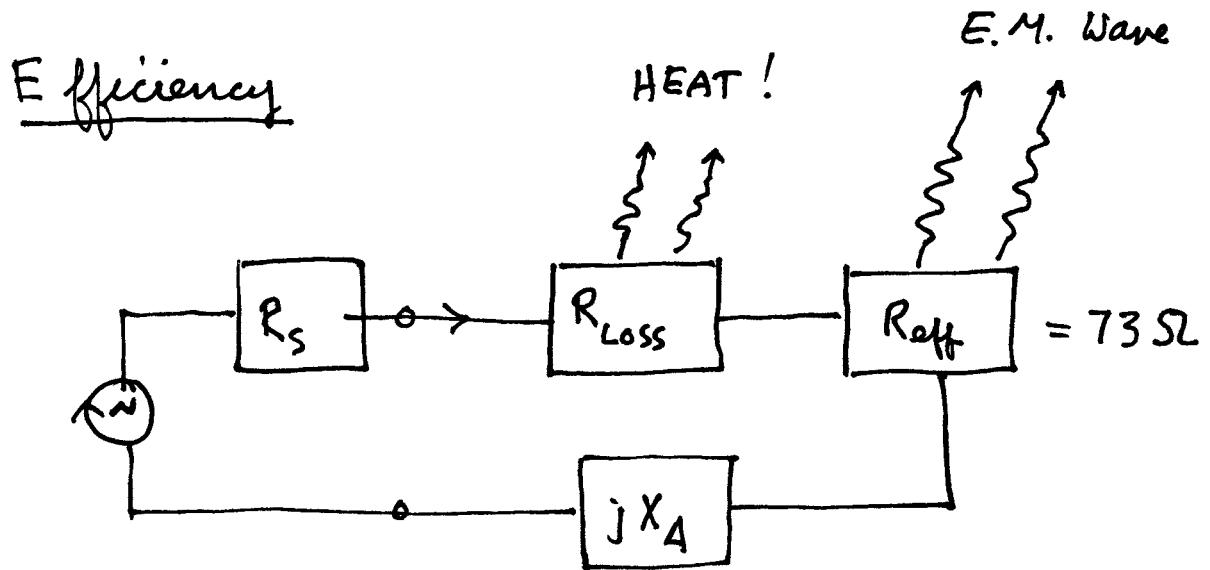
Radiation Resistance of $\lambda/2$ - Dipole

$$\frac{1}{2} |I_0|^2 R_{\text{eff}} = \gamma \frac{|I_0|^2}{4\pi} (1.219)$$

$$R_{\text{eff}} = \frac{120\pi}{2\pi} (1.219) = 60 \cdot 1.219 = \underline{\underline{73.52}}$$

$$Z_{\text{in}} = 73.52 + j \times (f) \quad \text{near } \frac{\lambda}{2} = l.$$

Consider the field diagrams in Kraus, pp 56-57.



$$\frac{P_{\text{rad}}}{P_{\text{TOT}}} = \left[\frac{R_{\text{eff}}}{R_{\text{LOSS}} + R_{\text{eff}}} \right] = \epsilon_A \quad \text{antenna efficiency}$$

for $l \leq \lambda/2$,

P_{rad} and $R_{\text{rad}} = R_{\text{eff}}$ are strongly dependent

on length $\left(\frac{\Delta z}{\lambda}\right)^2$ or $(l/\lambda)^2$,

while D_0 and A_{eff} are indifferent

to the length !

Radiation Characteristics
Compared

$$\frac{2}{\pi} \left| \frac{I_0}{2} \right|^2 (1.22)$$

	<u>Ideal</u> $D_3 \ll \lambda$	<u>Short</u> $\lambda \ll l$	<u>Half-wave</u> $\frac{\lambda}{2} = l$
P_{RAD}	$\frac{\pi}{3} \eta \left \frac{I_0 D_3}{\lambda} \right ^2$	$\frac{\pi}{3} \eta \left \frac{I_0 \lambda}{2\lambda} \right ^2$	$\frac{1}{4\pi} I_0 ^2 (1.22)$
D_o	$3/2$	$3/2$	1.643
A_{eff}	$3\lambda^2 / 8\pi$	$3\lambda^2 / 8\pi$	$\frac{3.2}{8\pi} \lambda^2$
$R_{eff} = R_{RAD}$	$80\pi^2 \left(\frac{D_3}{\lambda} \right)^2 S_2$ $789 \cdot (")^2$	$20\pi^2 \left(\frac{\lambda}{\lambda} \right)^2 S_2$ $197 \cdot (")^2$	7352